行政院原子能委員會

委託研究計畫研究報告

「大氣環境因子對太陽能預測與發電影響之研究」 A study of effects of atmospheric environmental factors to solar power forecasting and electricity generation

- 計畫編號: 1042001INER017
- 受委託機關(構):萬能科技大學
- 計畫主持人:王金印
- 聯絡電話:0953616429
- E-mail address : jywang@mail.vnu.edu.tw
- 核研所聯絡人員:馬志傑
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中文摘要

本計畫的目標為研究對太陽能預測與發電量影響之大氣環境因 子。太陽能預測所需的資料來源為日本地球同步衛星長期的可見光 資料,而大氣環境資料為核能研究所於龍潭、路竹、恆春等地區建 置之太陽能發電系統環境觀測站。研究內容為利用日本地球同步衛 星 MTSAT (Multi-functional Transport Satellite)長期的可見光資料建 立各區域晴空時全天空輻射(Global Horizontal Irradiation: GHI)量和 直射日照(Direct Normal Irradiation: DNI)量,再利用即時的衛星資料 計算台灣地區地面全天空輻射量。此外,探討在不同臭氧(ozone)、 水氣(water vapor)及氣膠(aerosol)含量下,全天空輻射量及直射日照 量的變化情形,以及對太陽能發電量的影響。

關鍵詞:日本地球同步衛星、氣膠、全天空輻射量、直射日照量

Abstract

The purpose of this project is to investigate the solar energy forecasting and environmental factors that affect the amounts of solar power generation. The data for solar energy forecasting were from Japanese Geostationary Satellite, MTSAT (Multi-functional Transport Satellite), visible image and the environmental data were from the Observation stations of Nuclear Energy Institute located at Longtan, Lujhu, and Hengchun. A long period of Japanese Geostationary satellite MTSAT visible data were used to obtain the backgrounds of Global Horizontal Irradiance and the Direct Normal Irradiance in clear weather situation. Under the given backgrounds, the ground Global Horizontal Irradiance in any weather situations was computed by using the real-time MTSAT visible data. In addition, under clear weather situations the variations of GHI and DNI with various amounts of ozone, water vapor, and aerosol were investigated and also their effects on solar power generation.

Keywords: Geostationary Satellite MTSAT, aerosol, Global Horizontal Irradiance, Direct Normal Irradiance

計畫主持人:王金印副教授 萬能科技大學資訊管理系 共同主持人:林宏志副教授 萬能科技大學電子工程系 共同主持人:李國路副教授 萬能科技大學管理與資訊系 共同主持人:陳萬金教授 大華科技大學電子工程系

壹、計畫緣起與目的

隨著能源短缺和環境污染的日益嚴重,能源問題已成為箝制經 濟發展的瓶頸,尤其是台灣在能源的支出方面,受到能源價格高漲 的影響,漸漸抵銷辛苦賺取的外匯,越來越多的國家開始開發可再 生的能源。由於太陽能資源取之不盡和清潔無污染的特性,已成為 開發新能源的首選。太陽能通常以光熱、光電、光化學方式轉換為 熱能、電能和化學能。

近年來,隨著太陽能應用產業的發展對於太陽能預報需求不斷 的增加,先進國家對於太陽能預報方法的研究發展得相關快速。國 外太陽輻射預報的方法主要有三類:(1)基於統計和類神經網路的預 測方法,可再細分為(a)基於即時和歷史數據的統計預報,這是一種 統計外推方法,相對簡單但僅適用於 0~1 小時內的鄰近預報;(b) 基於類神經網路的預測方法,但是利用天氣類型預報參數化來進行 太陽能預報,其預測時效與輸入的因子和數據有關,且預報結果具 有隨機性。這些統計方法主要是以時間序列為基礎,對於較長時間 的預測效果較差;(2)基於衛星雲圖資料的外推方法,能處理尺度較 小的對流雲系統,但由於天氣系統和相關雲系發展移動過程的非線 性,這種方法的預報時效為 0~5 小時;(3)利用數值天氣預報 (Numerical Weather Prediction, NWP)結果進行統計修正的方法,預 報時效可達數天。 然而太陽能發電系統的實際輸出功率主要受太陽輻射照度的影響,這是因為太陽輻射在時間上具有較大的不連續性和不穩定性。 它不僅受季節和地理因素的影響,而且與當時的大氣透明度、水氣 含量、氣膠(aerosol)、雲量、雲狀、雲與太陽的相對位置等有密切 相關。這裡的氣膠(微小顆粒物)是一個對太陽輻射有重要且複雜影 響的因素,它既可以直接反射、散射或吸收太陽輻射,又可以通過 改變雲的微物理性質而產生間接效應,同時不同氣膠之間對太陽輻 射的影響也有很大的差異。但總體而言,氣膠的增加通常還會使到 達地面的太陽輻射減少。

太陽輻射也同時受天文因素的影響,其變化又具有週期性,包 括日變化和年變化。其它環境因素如溫度等,對太陽輻射轉化效率 也會產生影響。太陽光發電系統併網運行以後,由於發電量的變化 是一個非平穩的隨機過程,輸出功率的不連續和不確定,會對電網 產生較大影響。因此,要想大幅提高太陽光發電量比例,降低運營 成本,保障電網安全,太陽能預報技術顯得尤為重要。對太陽能的 預報既要考慮太陽輻射的不穩定性,又考慮其週期性;考慮天文地 理因數的影響,又必須考慮氣象環境因數的影響。

本計畫即為配合核能研究所進行太陽光發電系統之技術發展相關研究之一。由於實際太陽能發電量取決於當時的大氣狀態,包括雲量、雲厚、臭氧及氣膠含量等。本計畫的目標為研究對太陽能預

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測與發電量影響之大氣環境因子。太陽能預測所需的資料來源為日 本地球同步衛星長期的可見光資料。研究內容為利用日本地球同步 衛星 MTSAT (Multi-functional Transport Satellite)長期的可見光資料 建立各區域晴空時全天空輻射(Global Horizontal Irradiation: GHI)量 和直射日照(Direct Normal Irradiation: DNI)量,再利用即時的衛星資 料計算台灣地區地面全天空輻射量。此外,探討在不同臭氧(ozone)、 水氣(water vapor)及氣膠(aerosol)含量下,全天空輻射量及直射日照 量的變化情形,以及對太陽能發電量的影響。

貳、研究方法與過程

一般分析影響太陽輻射傳輸到地球地面之因素可整理如表1所 示[1-4]。其中,天體的運轉係屬有規律的現象,可用數學模式精確 地掌握。故當對特定時間與地點進行太陽輻射量推算時,地理因素 與幾何因素也會特定下來,較難預測的只剩大氣狀況變化的影響。 因此,本部分的研究重點即在探討不同大氣特徵下,太陽輻射及直 射日照量的變化情形,以及作為探討其後對太陽能發電量的影響。

因素	來源
天文因素	A.地球—太陽距離。
	B.太陽赤緯(declination)(太陽入射線與赤道面之夾角)。
	C.時角(hour angle)(地球自轉每小時 15°)。
地理因素	A.緯度及經度。
	B.海拔高度。
	C.受輻射面之表面性質(表面之物理化學性質)。
幾何因素	A.太陽高度角及赤緯。
	B.受輻射面之周遭地形遮蔽效應。
	C.受輻射面之傾斜度(地形起伏的地形效應)。
	D.受輻射面之方位。
大氣因素	A.經過大氣時受到雲的影響。
	B.經過大氣時受到大氣分子、懸浮微粒、水氣的吸收、
	反射、與散射。

表1 影響地球接收太陽輻射量之因素

地球接收之太陽輻射量推算模式,主要可分物理模式與統計模

式雨類[5]。第一類是物理模式,考慮懸浮微粒、氣體分子、水氣、 雲滴等變數對於太陽輻射穿越大氣的吸收與散射等影響,然後計算 到達地面的太陽輻射量量值;而這些變數的大氣垂直分布剖面,是 由即時探空觀測或是實驗與氣候平均值提供;第二類為統計模式, 不考慮大氣輻射傳遞過程的細節,直接使用若干地面氣象參數與太 陽輻射的統計關係來快速計算太陽輻射量。精確的太陽能預報是基 於輻射傳輸理論,即太陽輻射穿過大氣層傳輸到達地面的物理過程, 包括雲、氣膠、水汽等對輻射的吸收、散射和反射的機理,通過地 面氣象觀測、高空大氣探測、衛星遙感、數值類比等手段獲得相關 要素的資訊,包括大氣透明度、水汽含量、氣膠、雲量、雲狀、溫

對於太陽能發電系統,尤其是高聚光型太陽能發電系統(High Concentration Photovoltaic, HCPV)的相關研究而言,了解特定地表的 直接日照量是一項非常重要的工作,因為它是 HCPV 系統中最主要 的能量來源。但是 DNI 主要會受雲、氣懸膠、水氣及臭氧等氣候 因素影響而產生變化,當然也對太陽能發的電量造成影響。為求逐 步了解氣候因素對 DNI 的變化影響,本部分的研究工作分成以下 三個部分:

一、探討晴空全天空太陽輻射變化情形

二、在先不考慮雲因子的條件下,僅以氣膠、水氣及臭氧等三種因

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子為重點,探討直射日照量的變化情形

三、探討直射日照量的變化情形對太陽能發電量的影響





圖 1 研究方法與流程圖

参、主要發現

一、國內外相關技術資料蒐集

2013 年 Academic Press 出版太陽光發電預報的專書[8],美國加 州大學聖地亞哥分校的 Jan Kleissl 教授主編,對太陽光發電預報提 出廣泛及系統化的介紹,太陽光發電預測,關鍵性地降低技術及財 務的風險,應用包含選擇地點、太陽光發電技術及併網供電考量, 在可行性分析階段、設計階段及部署階段都極為重要,不同的發電 技術,太陽光發電轉換效率自 6%提昇至 43%(1976 年至 2014 年), 參考圖 2:



圖 2 太陽光發電轉換效率

由於太陽光發電轉換效的提昇,太陽光發電逐漸被廣泛應用, 更併網到電力供應系統,然而太陽光發電本質上具有高變化特性, 在太陽光發電相關技術發展之中,太陽光的預測是一項關鍵議題。

2012 年美國加州大學聖地亞哥分校的 Hugo T.C. Pedro 發表論 文[9],討論在無外加輸入條件下的預測方法,於加州莫希地(Merced), 使用單軸追蹤, 1MW 太陽光發電,實驗時間 2009 年 11 月至 2011 年 8 月,收集每小時平均輸出,預測 1 至 2 小時之後的小時平均輸 出,使用 5 種常用的預測方法包含: Persistent model、Auto-Regressive Integrated Moving Average (ARIMA)、k-Nearest-Neighbors (kNNs)、 Artificial Neural Networks(ANNs)、ANNs optimized by Genetic Algorithms (GAs/ANN),預測結果統計預測值與量測值之差值,以 為平均絕對誤差(MAE)、平均偏移誤差(MBE)及關聯係數(R²)為基礎, 實驗時量測的部份數據用於訓練,部份數據用於驗證,如圖 3,陰 影部份用於訓練。





實驗結果發現以人工類神經網路(ANN)為基礎的預測法有較佳效果,參考表2及3,分別為1小時預測誤差及2小時預測的誤差,

表 2 一小時預測的誤差

statistical er	tatistical error metrics for the 1 h ahead forecasting for the several methodologies. The highlighted numbers identify the best performing method for a given error metric and variability period.																			
Model MAE (kW)			MBE (kW)		RMSE (kW)			nRMSE (%)			R^2									
	Tot	P_1	<i>P</i> ₂	<i>P</i> ₃	Tot	P_1	P_2	P ₃	Tot	P_1	P_2	<i>P</i> ₃	Tot	P_1	P_2	<i>P</i> ₃	Tot	P_1	<i>P</i> ₂	<i>P</i> ₃
Persistent	61.65	61.28	66.90	56.08	29.46	24.46	32.51	40.84	107.48	109.83	110.06	96.31	19.27	22.80	17.35	14.60	0.92	0.91	0.92	0.94
ARIMA	72.80	79.60	73.00	51.78	-0.50	-0.92	-0.52	0.80	105.68	115.57	104.24	69.77	18.95	23.99	16.43	10.58	0.92	0.90	0.93	0.97
(NN	61.92	71.65	69.15	22.94	-0.55	2.38	-4.51	-4.45	116.54	129.18	124.09	42.07	20.90	26.82	19.56	6.38	0.91	0.87	0.90	0.99
ANN	53.49	61.23	53.76	29.51	1.60	-1.61	0.34	13.01	88.23	98.22	87.63	47.21	15.82	20.39	13.81	7.16	0.95	0.93	0.95	0.98
GA/ANN	42.96	48.90	42.98	24.76	1.08	0.52	-2.08	6.85	72.86	80.56	72.45	42.19	13.07	16.72	11.42	6.40	0.96	0.95	0.97	0.99

表 3 雨小時預測的誤差

Statistical e	statistical error metrics for the 2 h ahead forecasting for the several methodologies. The highlighted numbers identify the best performing method for a given error metric and variability period.																			
Model MAE (kW)			MBE ()	MBE (kW)		RMSE (kW)			nRMSE (%)			R^2								
	Tot	<i>P</i> ₁	P_2	P_3	Tot	<i>P</i> ₁	P_2	<i>P</i> ₃	Tot	P_1	P_2	P ₃	Tot	P_1	P_2	P ₃	Tot	P_1	P_2	P_3
Persistent	91.12	91.74	95.32	83.88	44.19	37.84	45.47	61.92	160.79	164.33	160.93	149.29	28.86	34.11	25.36	22.70	0.83	0.79	0.83	0.85
ARIMA	102.76	113.83	102.76	68.96	-0.65	-1.90	-0.11	2.48	144.26	157.97	142.70	93.44	25.89	32.79	22.49	14.21	0.86	0.81	0.87	0.94
kNN	87.76	104.41	92.71	30.58	-3.44	-0.81	-8.08	-5.55	162.37	182.39	167.56	55.56	29.14	37.86	26.41	8.45	0.82	0.75	0.82	0.98
ANN	89.12	100.08	91.97	52.01	4.48	-6.80	8.84	33.36	142.74	154.34	149.64	85.26	25.61	32.04	23.58	12.96	0.86	0.82	0.85	0.95
GA/ANN	62.53	72.89	57.53	37.25	0.23	-0.68	-3.38	7.59	104.28	117.47	98.29	59.12	18.71	24.39	15.49	8.99	0.93	0.89	0.94	0.98

日照變化中等(2011.05.01 至 2011.06.30), P3 代表日照變化小 (2011.07.01至2011.08.15),實驗結果顯示ANN預測法有較佳效果, 其結構及參數可以基因演算法進一步優化。

2013 年美國加州大學聖地亞哥分校的 Ricardo Marquez[10], 討 論混合使用衛星影像及地面遙測作為人工類神經網路的輸入, 對全 日照執行 30 分鐘、60 分鐘、90 分鐘及 120 分鐘的預測,測試地點 在於加州莫希地(Merced)及戴維斯(Davis),使用衛星影像分析的速 度(velocimetry)及雲指標 cloud index,以及地面量測的全日照,作為 ANN 預測的輸入,在加州中央山谷地區在任何時間,影響全日照最 嚴重的因子是雲的覆蓋,然而,精準地預測雲的延申、移動、形成、 消失及變形,是複雜而不實際的工作,因此,發展混合使用衛星影 處理及 ANN 的預測 GHI 的方法,步驟摘要如圖 4,



圖 4 處理步驟

由衛星可見光影像,處理及計算出具有指標的雲影像(indexed image),由衛星紅外光影像,處理及計算出雲影像的速度向量,上 述兩步驟係平行處理,指標雲影像及雲影像的速度向量匯入人工類 神經網路,執行全日照的預測,ANN 分成三種結構,Ĝ_p假設雲指 標沒有變化,Ĝ_{f1}輸入未包含延遲的GHI,Ĝ_{f2}輸入包含延遲的GHI, 30 分鐘及 90 分鐘的預測分別如圖 5、6 所示。



圖 5 30 分鐘的預測



圖 6 90 分鐘的預測

其中, 左圖為Ĝ_p, 中間為Ĝ_{f1}, 右圖為Ĝ_{f2}, 三者的相關係數 R² 皆大於 0.85, 實驗可接受。預測誤差如表 4, 顯示預測時間愈短有 較準確的預測, ANN 結構若包含延遲的日照輸入, 則有更較準確的 預測。

表4 預測誤差

Forecast	MBE (w/m ²)				RMSE (w/m ²)	1-RMSE/RMSE _p (%)			
Horizon	Set	\widehat{G}_p	\widehat{G}_{f1}	\widehat{G}_{f2}	\widehat{G}_p	\widehat{G}_{f1}	\widehat{G}_{f2}	\widehat{G}_{f1}	\widehat{G}_{f2}
30 min.	Train/Val.	2.01	1.83	1.78	63.27	56.79	51.89	10.25	17.99
	Test	1.29	-7.22	-2.07	61.24	57.84	49.79	5.56	18.70
60 min.	Train/Val.	4.75	1.87	0.64	80.58	66.68	62.02	17.28	23.04
	Test	3.97	-7.06	-3.87	77.94	68.11	62.42	12.61	19.91
90 min.	Train/Val.	10.23	1.85	2.49	92.88	74.70	72.10	19.58	22.24
	Test	8.63	-6.08	-3.28	93.52	75.31	73.06	19.47	21.88
120 min.	Train/Val.	16.37	3.40	2.95	105.00	79.32	79.77	24.46	24.03
	Test	14.52	-2.26	0.01	107.47	80.21	81.26	25.27	24.39

2012 年美國加州大學聖地亞哥分校的 Hugo Yinghao Chu 發表 論文[11],討論實時預測前 10 分鐘的日照突波(ramp),預測值為 1 分鐘的平均值,日照突波通常引起發電量驟降,對單獨太陽光發電 及併網太陽光發電都是重要事件,日照量突然的變化,通常由雲的 遮蔽引起。本文實驗平台整合魚眼鏡頭的網路攝影機,使用雲追蹤 技術及 ANN 演算法,在加州海岸及大陸氣候地區各選一地點,收 集6個月的天空影像及日照資料,預測直接日照及全日照。實驗步 驟(1)雲辨識(2)產生具時序的雲指標(3)ANN 輸入訓練數據及雲指標 (4)評估預測結果。

突波的預測評估使用三參數, Ramp Detection Index (RDI)、False Ramp prediction Index(FRI)及 Ramp Magnitude index (RMI), 如表 5 °

表5 日照突波的預測

Location	Irradiance	Criteria	$0.1 < RM^* < 0.2~(\%)$	$0.2 < RM^* < 0.3$ (%)	$0.3 < RM^* < 0.5$ (%)	$RM^* > 0.5$ (%)
Folsom	GHI	RDI	23.50	43.40	55.00	67.30
		RMI	-25.00	12.70	24.50	30.00
	DNI	RDI	28.70	43.00	45.30	72.90
		RMI	-18.00	8.20	20.00	28.10
San Diego	GHI	RDI	26.60	35.60	52.40	65.90
		RMI	-21.00	-0.10	28.10	28.50
	DNI	RDI	19.40	42.40	45.00	69.80
		RMI	-30.00	5.80	15.90	25.10

圖 7 為大突波(RM* > 0.5)統計圖, (a) Folsom DNI(b) Folsom

GHI(c)San Diego DNI(d) San Diego GHI, 陰影為量測值, 黑色為預 測值。



圖 7 突波(RM*>0.5)統計圖

對直接日照突波的誤判在 Folsom 及 San Diego 分別為 2.6%及 4.2%,對全日照突波的誤判在 Folsom 及 San Diego 分別為 2.3%及 4.3%,大多數的誤判來自於雲的部份覆蓋。

小結:太陽光的預測是太陽光發電應用的關鍵,國內外相關技術資料顯示,在多種預測方法之中,收集量測資料,建立晴空日照參考基礎,混合使用衛星影像或地面天空影像及人工類神經網路是目前最準確的預測方法。

二、大氣環境因子對太陽能發電的影響之國外相關技術資料蒐集

在大氣環境因子對太陽能發電的影響方面,參考文獻提出操作 環境對太陽能發電效能的影響,太陽能發電(Photovoltaic, PV)的本 質,只有部份的太陽輻射被轉換成電能,剩下的照射被轉換成熱能, 從而提高 PV 模塊的溫度,並降低其性能,同時,遭遇操作環境的 影響。2015 年馬來西亞大學 Rahman 提出[12],以太陽輻射強度、 模組散熱能力、濕度及灰塵為參數,使用單晶太陽能發電模組,進 行室內實驗,顯示溫度每升高攝氏1度,發電效率降低0.06 百分點 如圖 8,相對濕度每增加10%,發電效率降低6百分點,0.012g/cm2 的灰塵使發電效率降低20百分點。



圖 8 溫度效應

2014 年阿爾吉利亞的再生能源中心發表論文[13],提出室外的 晴空測試結果,地點在非洲阿爾吉利亞的 Adrar 地區,實驗發現發 電效率與溫度成線性反比,發電效率與空氣質量(Air Mass)成線性反 比。灰塵或污漬(soiling)對太陽能發電的對衝擊十分明顯,2015 年 德國 Fraunhofer 太陽能系統學院 Schill [14]發表論文,室外測試大 西洋摩洛哥以西的 Canary island,5 個月之內,發電效率降低20 百 分點,期間下小雨使發電效率提高,下大雨使發電效率恢復如圖9。



三、可見光資料角度訂正處理

1. 太陽天頂角訂正

由於每一個地點的太陽能輻射量隨著時間的變化而不同,所以必須進行太陽天頂角訂正,按照球面三角學公式,可知

 $\cos\theta_0=\sin\delta_0\,\sin{\emptyset}+\cos\delta_0\,\cos{\emptyset}\,\cosh{h}$

其中 θ_0 , δ_0 , ϕ , δ_0 , h 分別為太陽天頂角(solar zenith angle)、 太陽赤緯(solar declination)、緯度(latitude)、時角(hour angle)。

本研究以2014 年台灣地區整年每天 8~17 時的 MTSAT 可見光 數位灰階值(visible digital count)先行太陽天頂角訂正,其天頂角訂 正的 Fortran 程式碼: sla-correction.f 請參閱附件二。然後求取密雲 的數位灰階值(意即可見光雲圖上最亮的點,代表反射最強的地方, UB)以及晴空的數位灰階值(意即可見光雲圖上最暗的點,代表反射 最弱的地方,LB),然後計算每個點的雲指數(cloud index)。

 $CI = \frac{UB - CCC}{UB - LB}$

四、各特定區域各季節地面全天空輻射量變動範圍計算

1. 抓取日本 MTSAT 氣象衛星可見光雲圖,並切割台灣位置影 像的步驟

步驟1:MTSAT 氣象衛星網址

ftp://mtsat.cr.chiba-u.ac.jp/grid-MTSAT-2.0/MTSAT2 步驟 2: 若要抓取 2015 年 2 月的資料,選擇 201502

- 步驟 3: 若要抓取 2015 年 2 月 8 日的資料,選擇 201502080001.vis.tar.bz2。2015 是年,02 是月,08 是日,00 是時,01 是分,vis 是可見光,tar 是壓縮, bz2 是壓縮
- 步驟 4: 解壓縮後檔案為 201502080001.vis,檔案大小為 288000000 bytes (=12000 X 12000X2),其資料格式 為 12000 X 12000 網格點的資料,每個網格點的數 值為 0~1023,使用 2 Bytes 儲存,而且是宣告為 沒有正負的資料格式。
- 步驟 5:為了能看到衛星影像,需要將網格點的數值由原來 0~1023 降為 0~255,也就是 2 bytes/pixel 轉成 1 byte/ pixel。處理上就是每個網格點的數值除以四, 再存為一新檔。

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步驟 6 : 切割台灣大小的影像(圖 10),原影像大小為 12000*12000,涵蓋範圍從東經 85.005 E 到西經 154.995 W,北緯 59.995 N 度到南緯 60.005 S。台 灣 範 圍 取 北 緯 25.505~21.755 N,東 經 119.005-123.005E 所以原影像中取第 3451-3780 條 掃描線,每條線取第 3501-3700 個 sample,每張台 灣影像為 350 (1ine) * 200(samples),緯度範圍 (25.505 N to 21.775 N, 376 1ines)。

切割台灣大小影像的 Fortran 程式碼: tw.f

```
read MTSAT gridded file with 12000 line by 12000 samples
С
   and get a subarea with 350 lines and 200 pixels per line.
С
   The upper left point is located at 22 degree N, 120 degree
С
   E. Grid size is 0.01 \times 0.01 degree.
С
   integer*2 m(12000)
   integer*1 m1(400)
С
   open(unit=2, file=
   'IMG DK02VIS 201502210201. geoss little', status='old',
   form='unformatted', access='direct', recl=24000)
   open(unit=3, file=' taiwan201502210201. raw',
С
   status='unknown', form='unformatted', access='direct',
С
   rec1=201)
С
      open(10, file='tw201502210201. dat', status='unknown')
   taiwan range 25.005~21.775 N and 119.005~123.005 E
С
   line from 3450 to 3825 and pixel from 3401 to 3800
С
   taiwan image size is 376 lines * 400 pixel
С
      do i=3450, 3825
          read(2, rec=j) (m(jj), jj=1, 12000)
          do k=3401, 3800, 10
             1 = k + 9
              write(10, 8)(m(11), 11=k, 1)
          enddo
      enddo
```

8

format(10i6)

stop

end

步驟 7:影像顯示及比對,影像比對,為確認處理的過程是 否正確,可抓取其網站影像圖檔比對其位置為 ftp://mtsat.cr.chiba-u.ac.jp/quicklooks/MTSAT2



圖 10 切割台灣大小的影像

2. 計算地面全天空輻射及直射日照量的變化情形

太陽輻射在地球大氣外可視為常數,但因地球有運行軌道,在 一年中的不同時間,地球大氣外某一地點與太陽的距離不相等,因 此照射到地球大氣外的太陽幅射(Extraterrestrial Radiation, ETR)須 加以修正,如圖 11 所示[15]。此外,地球大氣外太陽輻射經過大氣 層到達地球表面的過程中,受到太陽位置及大氣組成份子(如,臭氧、 水氣、氣膠及雲等)的干擾,對太陽光的穿透特性又會產生另一階 段的影響,如圖 12 所示[16]。本研究即在探討晴空(無雲)的情形下, 臭氧、水氣及氣膠對地面全天空輻射及直射日照量的變化情形。







圖 12 太陽位置及大氣組成份子對太陽輻射的干擾[16]

3. Bird and Hulstrom 模式

晴空模型通常使用不同的輻射傳送模型(RTM),以當地氣象 為輸入,諸如臭氧含量,水氣含量及與太陽的幾何位置,計算出給 定條件下的輻射,可選擇的模型有:Solis model、European Solar Radiation Atlas (ESRA) model、Bird and Hulstrom model、Molineaux model、Ineichen model、CPCR2 model、REST2 model、Kasten model、 Polynomial fit、ASCE evapotranspiration model 等多種。本研究部分 參考已被廣泛採用的 Bird and Hulstrom 模式[17,18],這是美國國 家能源部所發展的晴空日照模式,摘要如下:

(1)晴空直接日照(*DNI*_{clear})

$$DNI_{clear} = I_o R_c T_R T_o T_{UM} T_W T_A$$
⁽¹⁾

其中:

(a) *I_o*為地球大氣層外的太陽輻射,為一常數值(=1366
 W/m²)[19];

(b) *R*_c 為一修正值,作為地球隨運行軌道距離變化時的調整,因而地球大氣外太陽幅射 *ETR* 可透過 *R*_c 修正為:

$$ETR = I_0 R_c \tag{2}$$

而

$$R_c = 1 + 0.033 \cos(2\pi \, dn/365) \tag{3}$$

另 dn 是一年的第幾天(day number), 值為 1~365。

在式(1)中的 T_{R} 、 T_{o} 、 T_{UM} 、 T_{W} 、 T_{A} 分別代表雷利散射穿透率 (transmittance of Rayleigh scattering)、臭氧穿透率(transmittance of ozone absorptance)、 齊 一 混 合 氣 體 穿 透 率 (transmittance of absorptance of uniformly mixed gases)、水氣穿透率(transmittance of water-vapor absorptance)、 氣 膠 穿 透 率 (transmittance of aerosol absorptance)的係數,再分述如下:

(c) 雷利散射穿透率 TR

$$T_{R} = \exp(1 + M_{P} - M_{P}^{1.01})(-0.0903M_{P}^{0.84})$$
(4)

 m_p 為氣壓校正的大氣光程(Air Mass),

$$M_{P} = \frac{MP_{S}}{P_{O}}$$
(5)

$$M = \frac{1}{\cos(z)} \tag{6}$$

而 M 為大氣光程(Air Mass), z 是天頂角(Zenith Angle), $P_o = 1013$ milibar(mb), $P_s = P_o \exp(-0.000832h)$, h為站台高度,以 公里為單位,一般可用 $P_s \approx 0.99P_o \mathcal{B} M_P \approx \frac{M}{1013}$ 。 (d) 臭氧穿透率 T_o

$$T_{o} = 1 - 0.1611Ozm(1 + 139.48Ozm)^{-0.3035} - (0.002715Ozm)/(1 + 0.044Ozm + 0.0003Ozm^{2})$$
(7)

而 Ozm=OzM, Oz 為大氣臭氧柱總量(total column ozone amount) (at-cm)。

(e) 齊一混合氣體穿透率 TUM

$$T_{UM} = \exp(-0.017M_p^{0.26}) \tag{8}$$

(f) 水氣穿透率 T_w

$$T_W = 1 - 2.4959 W / \left[(1 + 79.034 W)^{0.6828} + 6.385 W \right]$$
(9)

而 W = PWM, PW 為可降水汽含量(perceptible water vapor) (atm-cm)。

$$T_A = \exp\left[(-\tau_A^{0.873})(1 + \tau_A - (\tau_A^{0.7088})M^{0.9108}]\right]$$
(10)

而 $\tau_A = 0.2758 \tau_{A,0.38} + 0.35 \tau_{A,0.5}$, $\tau_{A,0.38}$ 為 380nm 波長氣膠光學厚度

(Aerosol optical depth at 380nm), $\tau_{A,0.5}$ 為 500nm 波長氣膠光 學厚度(Aerosol optical depth at 500nm)。

$$GHI = \frac{I_b \cos(z) + I_{as}}{1 - A_b R_s} \tag{11}$$

其中:
(a)
$$I_b = DNI_{claer}$$
,

(b) *I*_{as}為在水平面的天空發散輻射(Sky scattered radiation on a horizontal surface),

$$I_{as} = D_s (0.5(1 - T_R) + 0.85(1 - T_A / TAA)) / (1 - M + M^{1.02})$$
(12)

(c) D_s 為天空擴散發散輻射 (Sky diffuse scattered radiation),

$$Ds = 0.79 I_o \cos(0.01745 z) T_o T_g T_W TAA$$
(13)

(d) T_g 為氣體光學特性穿透率(Transmittance due to optical properties of gases)

$$T_g = \exp(-0.0127 M_P^{0.26}) \tag{14}$$

(e) TAA 為氣膠吸收(Aerosol absorptance)

$$TAA = 1 - 0.1(1 - M + M^{1.06})(1 - T_A)$$
(15)

(f) R_s為反射天空輻射(Reflected sky radiation)

$$Rs = 0.0685 + (1 - Ba)(1 - T_a / TAA)$$
(16)

(g)Ab為地面反照率(albedo)。

由方程式(7)(9)(10)可畫出臭氧、水氣、氣膠的穿透率(transmittance)分別與天頂角的關係,如圖13~15所示,



圖 13 臭氧的穿透係數與天頂角(Ozone, 0-3.5cm)



圖 14 水氣的穿透係數與天頂角(Water Vapor, 0-6cm)



圖 15 氣膠的穿透係數與天頂角(AOD, 0-0.4)

初步觀察可得,在天頂角較大時,臭氧、水氣及氣膠的穿透率 有較大變化,對地面全天空輻射及直射日照有較大的影響。

(3) 範例實驗

使用上述 Bird Model, 在個人電腦以 Matlab 語言, 模擬計算晴空直接日照及晴空全日照, 可設定的參數如下:

名稱	說明	名稱	說明		
緯度(Latitude)	北緯為+	經度(Longitude)	東經為+		
	南緯為-		西經為-		
日數	一年第幾	時區(Time Zone)	台灣+8		
	天(1-365)				
臭氧(Ozone)	0-0.35(cm)	水氣(Water Vapor)	0-6.0(cm)		
氣膠光學深度	0-0.4	地面反照率	0-1		
(AOD @ 500 nm)		(Ground Albedo)			

當分別改變臭氧、水氣及氣膠之一來進行實驗,即可觀察 GHI

及 DNI 的變化狀況, 作法如下:

(a)實驗#1,改變臭氧,假設條件如下,

名稱	說明	名稱	說明
緯度(Latitude)	23	經度(Longitude)	120
	(北緯為+)		(東經為+)
日數	132(5 月 13	時區(Time Zone)	8
	日)		
臭氧(Ozone)	0-0.35(cm)	水 汽 (Water	1.5 (cm)
		Vapor)	
氣膠光學深度	0.1	地面反照率	0.2
(AOD @ 500 nm)		(Ground Albedo)	

臭氧變化 0-0.35cm, 得 5 月 13 日 24 小時的 GHI 及 DNI 分別 如圖 16A 及 16B, 臭氧的影響日照最強時, 對應 GHI 的最大值及最 小值為(1063,1044)差值 19, DNI 的最大值及最小值為(939,921)差值 18。





圖 16B DNI

(b)實驗#2,水氣變化,假設條件,

名稱 說明 名稱 說明	
-------------	--

緯度(Latitude)	23	經度(Longitude)	120
	(北緯為+)		(東經為+)
日數	132(5 月	時區(Time Zone)	8
	13 日)		
臭氧(Ozone)	0.3	水氣(Water	0-6 (cm)
		Vapor)	
氣膠光學深度	0.1	地面反照率	0.2
(AOD @ 500 nm)		(Ground Albedo)	

水氣 0-6cm, 得 5 月 13 日 24 小時的 GHI、DNI 分別如圖 17A 及 17B, 日照最強時, 對應 GHI 的最大值及最小值為(1165,1002)差 值 163, DNI 的最大值及最小值為(1031,885)差值 146。



(c) 實驗#3, 氣膠光學深度變化, 假設條件,

名稱	說明	名稱	說明
緯度(Latitude)	23	經度(Longitude)	120
	(北緯為+)		(東經為+)
日數	132(5月13	時區(Time Zone)	8
	日)		
臭氧(Ozone)	0.3	水 氣 (Water	1.5 (cm)
		Vapor)	
氣膠光學深度	0-0.35	地面反照率	0.2
(AOD @ 500 nm)		(Ground Albedo)	

AOD 0-0.35, 得 5 月 13 日 24 小時的 GHI、DNI 分別如圖 18A 及 18B, 日照最強時, 對應 GHI 的最大值及最小值為(1073,1003)差 值 70, DNI 的最大值及最小值為(1017,772) 差值 245。



圖 18A GHI

圖 18B DNI

(d) 實驗#4,計算全年 GHI 等高圖及 DNI 等高圖,假設條件,臭氧、水氣、氣膠光學深度皆為零

名稱	說明	名稱	說明
緯度(Latitude)	北緯為+	經度(Longitude)	東經為+
	南緯為-		西經為-
	23		120
日數	1~365	時區(Time Zone)	8
臭氧(Ozone)	0	水 氣 (Water	0 (cm)
		Vapor)	
氣膠光學深度	0	地面反照率	0.2
(AOD @ 500 nm)		(Ground Albedo)	

計算全年的 GHI 等高圖及 DNI 等高圖,如圖 19A 及 19B,橫 軸表示時間,縱軸為全年的第幾天,色碼表示輻射(W/m²),



圖19A 全年的GHI 等高圖

圖19B 全年的DNI等高圖

(4) 日射量模擬模型

本方法以太陽的位置為基礎,可計算出地球任意位置的水平面 上輻射量。利用此方法可模擬日射量資料不足之區域,產生接近實 際量測的每小時日射輻射量,作為其他模式驗證比對或預測修訂之 用。此模擬法可分成以下七個步驟進行[20,21],說明如下: (a)計算出太陽的赤緯角(Declination) δ 太陽赤緯度可由式 2.1 得到,或由式 2.2 利用 Fourier 級數 產生。 $\delta = 23.45^{\circ} \sin t$ (17) $\delta = A_0 + A_1 \cos t + A_2 \cos 2t + A_3 \cos 3t + B_1 \sin t + B_2 \sin 2t + B_2 \sin 2t$ $B_3 sin 3t$ (18)其中 t=360°(nd - 80) / 365, nd 為日序:1月1日為1, 12 月31日為365。經由Fourier級數得知之係數A₀=0.386470, $A_1 = -0.792624$, $A_2 = 0.377853$, $A_3 = 0.030124$, $B_1 = 23.259526$, $B_2=0.131544$, $B_3=-0.167013$ °

(b) 計算出太陽的時角(Hour angle)ω
 在一天的 H 時之時角為:
 ω = 15° · (H −12)
 (19)

(c) 計算出太陽的仰角(Elevation) α ,天頂角(Zenith Angle) θz ,方位角(Azimuth) ζ 在緯度為ん時: $\Theta z = \cos^{-1}(\cos\lambda\cos\delta\cos\omega + \sin\lambda\sin\delta)$ (20)

$$\boldsymbol{\alpha} = 90^{\circ} - \theta z \tag{21}$$

$$\zeta = \sin^{-1}(\cos\delta\sin\omega) / \sin\theta z \tag{22}$$

(d) 計算出晴空時太陽光束在(1)水平面上全般輻射量 Gc、
(2)垂直面上全般輻射量 Ic、(3)水平面之散射量 Dc

$$G_c = p \sum_{s=0}^{6} Q_s y^{2s} \qquad s = 1, 2, \dots, 6$$
(23)

$$I_c = p \sum_{s=0}^{6} R_s y^{2s} \qquad s = 1, 2, \dots, 6$$
(24)

$$D_c = G_c - I_c \cos \theta_z \tag{25}$$

其中 $p=1-0.0335\sin 360(n_d - 94) / 365$, $y = \frac{\theta z}{90^\circ} Q Q R$ 的係數為:

$Q_0 = 1.1049$	$R_0 = 0.9864$
$Q_1 = -1.4354$	$R_1 = -0.2001$
$Q_2 = -1.0720$	$R_2 = -1.1883$
$Q_3 = 6.6849$	$R_3 = 3.3705$
Q_4 = -13.8990	R_4 = -5.7674
$Q_5 = 13.0798$	$R_5 = 3.7206$
$Q_6 = -4.4631$	$R_6 = -0.9217$

(e) 計算出晴空時日全般輻射量 H_c

S_i	1	2	3	4
1	26.789453	-0.760391	-0.265078	-0.007734
2	0.092481	-0.050012	0.004731	-0.006719
3	1.209688	-0.025625	-0.008438	-0.005625
4	0.018456	-0.025926	-0.013168	0.015157
5	3.172571	2.431523	0.008367	-0.012203
6	0.112969	0.075469	0.007031	-0.037969
---	-----------	----------	----------	-----------
7	-0.064616	0.071846	0.005554	-0.037515

(f) 計算日晴空因子(K_d),時晴空因子(K_h): $K_d = G/H_c$ (27)

其 Ka 為水平面上的日晴空因子,即在地表水平面上日輻射量與 晴空時日全般輻射量之比值,G 是從中央氣象局提供的日輻射量。

Ka會隨時受大氣層內雲、水氣、懸浮粒子等影響,為模擬此種 大氣之隨機現象,可將Ka設為一個二項式分佈函數的"成功"機率; n 設為 10,代表 10 種大氣因子的覆蓋等級;再進行 0 與 1 間的隨機 亂數模擬二項式分佈的累積機率,透過函數倒推得到"成功個數" x 的值,進而求出每小時之晴空因子Kh:

K_h = x/n (28)
 若 K_h為 1 時表完全晴空,則 K_h為 0 時便表示天空完全
 被雲覆蓋。

(g) 計算出在水平面上第 i 小時之(1)輻射量(G_h)i、(2)擴充
 輻射量之比例(J_i)、(3)散射量(D_h)i、(4)直射量(I_h)i

$$(G_h)_i = (K_h)_i \times G_C \tag{29}$$

$$J_i = 1 - (I_C/G_C) \times \cos\theta z \tag{30}$$

$$(D_h)_i = [1 - (0.733(K_h)_i^2 + 0.267(K_h)_i^4)(1 - J_i)] \times (G_h)_i$$
(31)

$$(I_h)_i = ((G_h)_i - (D_h)_i)/\cos\theta_{zi}$$
(32)

以上複雜的計算,其日射模擬中重要變數之關係圖如圖 20 所示。 而日射模型與其他模型的水平面上之全輻射量綜合比較可如圖 21 所示。



圖 20 日射模擬中重要變數之關係圖



圖 21 日射模型綜合比較圖

3. 氣膠含量的計算

圖 22 為台灣地區 2015 年 6 月 1-8 日的氣膠分布,圖 23 為台灣 地區 2015 年 1 月氣膠分布,圖 24 為台灣地區 2015 年 3 月的氣 膠分布,圖 25 為台灣地區 2014 年的氣膠分布。



圖 22 台灣地區 2015 年 6 月 1-8 日的氣膠分布



圖 23 台灣地區 2015 年 1 月氣膠分布



圖 24 台灣地區 2015 年 3 月的氣膠分布



圖 25 台灣地區 2014 年的氣膠分布

五、地面晴空反射率和雲種的反射率計算衛星視場之雲指數

氣象衛星可見光雲圖,每一像素分為256 灰階值,以天頂角 校正的灰階值(Cosine-Corrected Count, CCC),每一像素計算雲指數 (Cloud Index, CI)計算為: $CI = \frac{UB - CCC}{UB - LB}$ 其中,UB 為最大值,LB 為最小值,由中央氣象局下載 (2015/08/31/09/00)的衛星影像如圖26,



圖 26 衛星影像(2015/08/31/09/00)

計算雲指數如圖 27, CI 值 0 至 1, 高的雲指數值表示雲層很厚, 遮蔽效果很強。



圖 27 雲指數

六、台灣地區地面全天空輻射量影像

以常規化全日照探討晴空全日照受到雲層遮蔽的結果,其中, $GHI_n = GHI_{clear} * (1 - CI)$

GHI clear 為晴空全日照,可由前述模式計算獲得,概念上雲指數是一項衰減系數,由圖 27 雲指數計算得到常規化全日照如圖 28。



圖 28 常規化全日照

本研究採用中央氣象局地面輻射觀測站的資料進行結果驗證, 表 6 為台北、台中、台南及花蓮四個測站的高度及經緯度位置;表 7 為 2015 年 8 月台北測站地面逐時的 GHI 觀測值。圖 29 為 2015 年 8 月台北測站地面逐時的 GHI 觀測值與衛星 GHI 反演值的散佈 圖,其相關係數為 0.87,樣本數為 620 個。圖 30 為 2015 年 8 月台 中測站地面逐時的 GHI 觀測值與衛星 GHI 反演值的散佈圖,其相 關係數為 0.85,樣本數為 620 個。圖 31 為 2015 年 8 月台南測站地 面逐時的 GHI 觀測值與衛星 GHI 反演值的散佈圖,其相關係數為 0.90,樣本數為 620 個。圖 32 為 2015 年 8 月花蓮測站地面逐時的 GHI 觀測值與衛星 GHI 反演值的散佈圖,其相關係數為 0.89,樣本 數為 620 個。

測站	測站編碼	測站海拔(公尺)	經度([°] E)	緯度 (°N)
台北	466920	7.0	121. 5149	25.0377
台中	467490	85.0	120.6841	24.1457
台南	467410	41.0	120.2048	22.9932
花蓮	466990	16.0	121.6133	23.9751

表 6 台北、台中、台南及花蓮四個測站的高度及經緯度位置

表7 2015年8月台北测站地面逐時的 GHI 觀測值

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				1	04/	/8	CWE	8-4669	20(Ta:	ipei)	GHI g	ground	i obse	ervati	on			U	nit:W	/m^2						
day	hour	01	02	03	04	05	06	07	08	09	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	мах
C)1	0	0	() () () (136.14	375.08	569.57	786.29	825.18	997.45	1000.22	902.98	641.81	341.74	244.5	102.8	0	0	0	0	0	0	1000.22
C)2	0	0	() () ()	113.91	338.96	547.34	677.93	697.38	864.08	791.84	627.92	297.29	263.95	169.48	116.69	0	0	0	0	0	0	864.08
C)3	0	0	() () ()	119.47	272.28	561.24	766.84	891.87	741.83	769.62	650.15	202.82	375.08	166.7	77.8	0	0	0	0	0	0	891.87
0)4	0	0	() () ()	127.81	361.19	541.79	583.46	758.5	989.11	964.1	891.87	102.8	111.14	52.79	0	0	0	0	0	0	0	989.11
0)5	0	0	() () ()	125.03	352.86	555.68	647.37	616.8	972.44	733.5	402.87	38.9	80.57	125.03	108.36	0	0	0	0	0	0	972.44
0)6	0	0	() () ()	155.59	305.62	575.13	611.25	925.21	944.66	978	952.99	791.84	539.01	325.07	100.02	0	0	0	0	0	0	978
C)7	0	0	() () ()	86.13	316.74	641.81	736.28	941.88	655.7	830.74	494.56	527.9	261.17	94.47	5.56	0	0	0	0	0	0	941.88
0)8	0	0	() () () (0 (2.78	75.02	127.81	177.82	172.26	275.06	280.62	166.7	88.91	0	0	0	0	0	0	0	0	280.62
0)9	0	0	() () ()	0 0	0	83.35	250.06	502.89	430.65	494.56	219.49	172.26	169.48	166.7	5.56	0	0	0	0	0	0	502.89
1	10	0	0	() () ()) 102.8	350.08	402.87	455.66	666.82	800.18	761.28	577.91	550.12	158.37	41.68	0	0	0	0	0	0	0	800.18
1	11	0	0	() () () () 144.48	341.74	552.9	744.61	694.6	897.42	925.21	661.26	405.65	8.34	0	0	0	0	0	0	0	0	925.21
1	12	0	0	() () () (91.69	288.95	536.23	750.17	922.43	908.54	661.26	686.26	327.85	27.78	0	0	0	0	0	0	0	0	922.43
1	13	0	0	() () () () 69.46	366.75	555.68	733.5	908.54	989.11	508.45	33.34	0	8.34	122.25	33.34	0	0	0	0	0	0	989.11
1	14	0	0	() () () (25.01	250.06	511.23	897.42	691.82	647.37	136.14	288.95	227.83	291.73	158.37	0	0	0	0	0	0	0	897.42
1	15	0	0	() () () (22.23	252.83	530.67	666.82	777.95	822.41	672.37	294.51	333.41	238.94	166.7	47.23	0	0	0	0	0	0	822.41
1	16	0	0	() () () (0 0	166.7	341.74	533.45	327.85	255.61	102.8	133.36	166.7	166.7	166.7	50.01	0	0	0	0	0	0	533.45
1	17	0	0	() () () (0 0	52.79	227.83	297.29	441.77	275.06	708.49	564.02	436.21	294.51	177.82	66.68	0	0	0	0	0	0	708.49
1	18	0	0	() () () () 141.7	61.12	352.86	591.8	491.78	333.41	397.31	269.5	41.68	0	0	0	0	0	0	0	0	0	591.8
1	19	0	0	() () () (133.36	369.53	589.02	780.73	922.43	964.1	847.41	905.76	680.71	280.62	305.62	108.36	0	0	0	0	0	0	964.1
2	20	0	0	() () () () 147.26	383.42	472.33	733.5	927.99	994.67	997.45	950.21	786.29	525.12	291.73	77.8	0	0	0	0	0	0	997.45
2	21	0	0	() () () (130.58	344.52	583.46	605.69	847.41	1011.34	644.59	689.04	672.37	427.87	255.61	72.24	0	0	0	0	0	0	1011.34
2	22	0	0	() () () (97.24	352.86	489	614.03	880.75	877.97	702.94	891.87	505.67	516.78	241.72	2.78	0	0	0	0	0	0	891.87
2	23	0	0	() () () (0 0	113.91	91.69	347.3	280.62	180.6	380.64	480.66	144.48	72.24	13.89	0	0	0	0	0	0	0	480.66
2	24	0	0	() () () (0 0	50.01	172.26	305.62	294.51	652.92	730.72	380.64	558.46	600.13	252.83	105.58	0	0	0	0	0	0	730.72
2	25	0	0	() () () (0 0	0	0	188.93	277.84	500.11	394.53	427.87	602.91	372.31	200.04	11.11	0	0	0	0	0	0	602.91
2	26	0	0	() () (0 0	141.7	186.15	422.32	441.77	486.22	211.16	316.74	302.85	166.7	108.36	0	0	0	0	0	0	0	486.22
2	27	0	0	() (0 0	0	125.03	211.16	338.96	505.67	141.7	0	0	0	61.12	0	0	0	0	0	0	0	505.67
2	28	0	0		<u>) (</u>	1		0 69.46	166.7	180.6	250.06	166.7	213.94	116.69	72.24	0	0	0	0	0	0	0	0	0		250.06
2	29	0	0	() (0 1	0	155.59	166.7	3/2.31	591.8	558.46	230.61	122.25	77.8	0	0	0	0	0	0	0	0	591.8
	50	0	0					0	180.6	166.7	311.18	313.96	286.18	113.91	191.71	77.8	144.48	0	0	0	0	0	0	0	0	313.96
A	VE	0	0	0	0 0) () 56.371	127.77	188.11	209.12	245.19	263.56	258.88	91.69 250.42	214.86	148.95	88.202	39.412	0	0	0	0	0	0	150.03



圖 29 為 2015 年 8 月台北測站地面逐時的 GHI 觀測值與衛星 GHI 反演值的散佈圖,其相關係數為 0.87,樣本數為 620 個。



圖 30 為 2015 年 8 月台中測站地面逐時的 GHI 觀測值與衛星 GHI 反演值的散佈圖,其相關係數為 0.85,樣本數為 620 個。



圖 31 為 2015 年 8 月台南測站地面逐時的 GHI 觀測值與衛星 GHI 反演值的散佈圖,其相關係數為 0.90,樣本數為 620 個。



圖 32 為 2015 年 8 月花蓮測站地面逐時的 GHI 觀測值與衛星 GHI 反演值的散佈圖,其相關係數為 0.89,樣本數為 620 個。

圖 33 顯示 2015 年 8 月份 GHI (MJ/m² * month)衛星反演值分布 圖,靠近台北、台中、台南及花蓮四個地面觀測站的衛星反演值分 別為 421.90,384.70,417.90 和 452.7 (MJ/m²)。表 8 顯示 2014 年 9 月至 2015 年 8 月台北、台中、台南及花蓮四個地面觀測站 GHI 月 觀測累積值(MJ/m²)。衛星反演值與觀測值比較顯示:相對於台北 觀測站,衛星反演值低估 8.7%;相對於台中觀測站,衛星反演值高 估 0.6%;相對於台南觀測站,衛星反演值低估 8.8%;相對於花蓮 觀測站,衛星反演值高估 1.7%。由此結果顯示衛星反演值與地面觀 測值相當一致,因此衛星的反演值在電力的管理上是相當可行的。



圖 33 2015 年 8 月 GHI (MJ/m^2* month)衛星反演值分布圖

表8 2014年9月至 2015年8月台北、台中、台南及花蓮四個地 面觀測站 GHI 月觀測累積值(MJ/m²)

Month	2014	2014	2014	2014	2015	2015	2015	2015	2015	2015	2015	2015
Station	/9	/ 10	/ 11	/ 12	/ 1	/ 2	/ 3	/ 4	/ 5	/ 6	/ 7	/ 8
Taipei	547.4	382.7	263.1	185.1	261.7	270.7	281.7	422.3	376.5	537.3	606.5	462.4
Taichung	458.3	488.2	337.4	260.8	364.3	363.1	369.8	516.2	392.6	549.5	489.4	382.3
Tainan	563.1	598.4	428.1	310.9	400.4	416.7	483.9	600.2	541.5	722.2	572.0	458.2
Hualien	532.5	377.0	276.2	138.1	198.3	220.2	275.6	342.7	446.7	601.4	606.8	445.0

七、太陽能發電量的環境因子影響分析

本研究計畫屬於多年延續性研究性質,此項的初步分析研究已 於 102 年度的計畫結案報告中[26],運用路竹太陽能發電之相關資 料,進行相關係數分析、主成份分析、因素分析、迴歸分析、與自 我相關排除等統計推論技術,針對環境因子影響,獲得最終的發電 量迴歸模式可寫成:

(直流電)i = -112.106+(348.214*全日照+2803.328*直射日照+20.997
*最大風速+63.551*大氣溫度-3.346*相對溼度)i+(0.736
直流電-256.286*全日照-2063.249*直射日照-15.454*最
大風速-46.774*大氣溫度+2.463*相對溼度)i-1

本節中進一步研究晴空全天空太陽輻射及直射日照量在不同臭氧、水氣及氣膠含量下的變化情形,結合這些環境因子分析,將更有助於太陽光發電預報的完整性,其成果可提供系統效能提昇及作為未來新建系統設計精進之參考。

以上述 Bird and Hulstrom 模式為例,輸入路竹區的經緯度 120.255⁰與22.837⁰,模式參數假設如表9,則5月13日的 GHI 與 DHI 產生如表 10 所示。

表9 Bird and Hulstrom 模式參數假設(地點:路	竹示	範場)
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名稱	說明	名稱	說明
緯度(Latitude)	22.837	經度(Longitude)	120.255
	(北緯為+)		(東經為+)
日數	132 (5 月 13 日)	時區(Time Zone)	8
臭氧(Ozone)	0.27	水氣	1.5 (cm)

		(Water Vapor)	
氣膠光學深度	0.35	地面反照率	0.2
(AOD @500 nm)		(Ground Albedo)	

表 10 路竹示範場區 5月 13 日的 GHI 與 DHI 值

小時(起點)	DHI	GHI
6	0.295	3.064
7	94.458	198.101
8	281.475	430.127
9	474.343	646.164
10	639.276	824.868
11	757.072	950.707
12	816.048	1013.323
13	810.739	1007.694
14	741.625	934.268
15	615.161	798.952
16	444.113	612.953
17	249.268	392.664
18	68.857	160.672

註:(只顯示大於0的部分)

當考量受環境因素影響的太陽光發電迴歸模式,進一步結合在 不同臭氧、水氣及氣膠含量下的變化情形,完成的5月13日之路 竹示範場某發電機座直流電預測值如表11所示,並繪出如圖34。 其中,全日照與直射日照值來自考量臭氧、水氣及氣膠含量的Bird and Hulstrom 模式,最大風速、大氣溫度、與相對溼度在此為假設值,其可依實地量測獲得。

小時(起點)	全日照	直射日照	最大風速	大氣溫 度	相對溼度	直流電
6	0.000	0.003	5.602	18.81	70.5	-
7	0.094	0.198	4.296	19.01	69.1	744.045
8	0.281	0.430	6.417	19.04	68.8	1635.570
9	0.474	0.646	5.982	18.95	69.1	2387.022
10	0.639	0.825	4.242	19.00	68.8	2982.797
11	0.757	0.951	4.922	18.96	70.0	3435.592
12	0.816	1.013	4.840	19.15	68.8	3683.563
13	0.811	1.008	5.357	19.32	67.5	3719.658
14	0.742	0.934	5.139	19.26	68.6	3498.271
15	0.615	0.799	6.200	19.33	67.8	3119.234
16	0.444	0.613	5.384	19.54	67.4	2546.903
17	0.249	0.393	5.438	19.62	67.4	1875.772
18	0.069	0.161	5.574	19.63	67.8	1170.944

表 11 結合臭氧、水氣及氣膠含量變化的太陽光發電預測



圖 34 5月 13 日路竹示範場某發電機座直流電預測值時圖

肆、結論

本研究完成獲取 TOMS 衛星資料所計算台灣地區臭氧含量分 布,計算臭氧的透射率,研究其對太陽能發電的影響。完成獲取 Aqua 及 Terra 衛星上 MODIS 所計算台灣地區之氣膠光學厚度(AOD), 計算氣膠的透射率,研究其對太陽能發電的影響。進一步利用 MTSAT 衛星可見光反射率計算台灣地區 10 km *10 km 內之雲量, 研究天空雲量對太陽能入射地面輻射量之影響。對於國際發展現況, 蒐集相關之大氣環境因子對太陽能預測與發電影響的資料分析與討 論。

本研究已完成由 MTSAT 衛星可見光資料反演自 2014 年 9 月 至 2015 年 8 月一整年的 GHI 的資料庫,反演的結果顯示衛星 GHI 反演值的分佈和地面觀測具有一致性。個別反演點位置和觀測點位 置的比較也顯示良好的相關係,對台北、台中、台南及花蓮等四個 測站其相關係數皆大於 0.85,而其 GHI 月累積量的反演值誤差也 小於 9%。對於未來供電要求,我們需要利用數值天氣預報模式預 測太陽能,例如天氣研究和預測 (WRF) 模型。但在當前的狀態 GHI 預測不夠好,需要更多的改善。圖 35 是 GHI 36 小時預測 2015 年 6 月 1 日 12 時 1 分的一個例子。結果表明,預測的 GHI 值 有高估的情況。為了改善其準確度,未來可使用 Ineichen SOLIS 模 式取代目前簡化的模型,其中將取用 MODIS 總水汽含量與氣膠光

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學厚度產品,這將提升 GHI 的準確性。



119E 119.5E 120E 120.5E 121E 121.5E 122E 122.5E

圖 35 利用WRF 模式預測36小時,模擬2015年6月1日12時1分的GHI (W/m^2) 分布圖

至於在太陽能發電方面,可以上述的環境因子對太陽能預測結 果,乘上設定的發電效率得到發電量理論值。至於大氣環境因子對 太陽能發電的影響,除上述的環境因子對太陽能預測影響之外,尚 涉及發電技術的問題,亦即等同於預測的太陽能乘以發電效率的問 題。

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附件一: SCI投稿

Global Horizontal Irradiance Retrievals by MTSAT data Over Taiwan Area

Jin-Yinn Wang¹, Wann-Jin Chen²*, Horng-Jyh Lin¹, Gwo-Luh Lee¹,

I-Tao Lung³, Chih-Chieh Ma³, Wan-Li Hsu³

¹Vanung University of Science and Technology, Taiwan

²Ta Hwa University of Science and Technology, Taiwan

³Institute of Nuclear Energy Research, Atomic Energy Council,

Taiwan

²* <u>wjchen@tust.edu.tw</u>

Abstract

One year Multifunctional Transport Satellite (MTSAT) visible data, from September of 2014 to August of 2015, were used to retrieve the Global Horizontal Irradiance (GHI) over Taiwan area. The Ineichen simplified SOLIS model was accepted to find the clear GHI, and the cloud index method was used to calculate the transparency of cloud. Combining the above two techniques, the observed satellite visible data were to converted into the GHI value for each pixel in the satellite image. There are four ground solar GHI stations' measurements were used to validate the satellite-derived GHI. The results show that the satellite GHI retrievals and the ground observations have a good relationship, with the correlation coefficients large than 0.85 for Taipei, Taichung, Tainan, and Hualien stations. The monthly satellite GHI retrievals are all comparable with those of observations under 9% difference for the above four stations.

Keywords: satellite retrieval, GHI, global horizontal irradiance, solar zenith angle, aerosol optical depth, air mass

1. Introduction

The climate of the world was changed significantly in the past few decades due to the global warming caused by the increasing carbon dioxide amounts produced by burning fossil fuels [1]. Carbon dioxide should be cut down by using renewable energies, like solar energy, wind energy, and reducing the usage of fossil fuel for human's sustainable developments. However, due to the unstable characteristics of the solar energy, the prediction of solar radiation will become a major issue in the integration of the upcoming solar energy resource into existing energy supply structure. Typically, the solar energy forecasting is divided into three kinds of terms according to time range, including very short term (sub-hourly), short term (sub-hourly to six hours) and long term (six hours to two days) forecasting. For very short term forecasting, a total sky imager is required to obtain cloud amounts and then calculate the cloud index and surface solar irradiance with given aerosol and haze amounts information. For example, Chow et al., [2] used a rooftop mounted TSI (Total Sky Imager) 440A to estimate sub-hourly direct normal irradiance forecasting at the UC San Diego (UCSD) solar energy test-bed. Chow made a conclusion that the use of sky imagery to assess the solar resource for solar energy applications shows much potential for augmenting the spatial and temporal resolution provided by satellite and numerical forecasting methods. For short term forecasting, geostationary satellite images are required to estimate cloud amounts and consecutive images to derive the wind direction and speed. For example, used Heliosat method, a semi-empirical method to derive solar irradiance from satellite data. For long term forecasting, a numerical weather prediction (NWP) model is needed to provide cloud information, including cloud amount, cloud type and cloud motion [3-5].

Cano et al. [6] presented a statistical method for the determination of the global solar radiation at ground level by using data from meteorological satellites. These results clearly demonstrate that satellite data can be used successfully for mapping both the global radiation at ground level and the cloud coverage over very large areas, with a ground resolution of 5 km x 5 km. The scheme was then upgraded by Beyer et al. [7], Hammer et al. [8], Rigollier et al. [9], and Durr and Zelenka [10].

Taiwan is a small island with 36,000 km² area but has a total of 23

million population. Though owning limit natural power resources, it is active in industrial production and economic activity and therefore makes huge energy consumption, resulting in more than 98% of energy needs by imports. Facing the global climate change, as one of the members of Earth village, Taiwan is asked to reduce the production of carbon dioxide. Therefore the government in Taiwan raises one "Sun roof of one million" project, aiming to produce 847 MW, 2120 MW, and 6200 MW photovoltaic power generation capacity in 2015, 2020 and 2030 respectively. The goal of this project is to create green industrials, to protect the global environment and to have a sustainable development of people's life in Taiwan. Fortunately, Taiwan is located between 22 °N to 25 °N, belonging to sub-tropical climate regions, having abundant solar energy resources, and thus brings the residents of a profound expectation: solar energy can replace a large part of future energy demand.

There are some researches on solar radiation in Taiwan. For example, Lin and Su [11] developed a simply method to estimate the monthly solar radiation for the purpose of physical environment design of architecture. They evaluated the solar radiation with 6 radiation observation measurements and concluded that there is a high correlation

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coefficient ($0.75 \sim 0.96$) between observations and predicted values. Chang [12] and Kao [13] both used the ground radiation measurements of Central Weather Bureau in Taiwan to study the properties of monthly averaged solar radiation and found that in temporal distribution the solar radiation has maximum value in July and minimum in January, in spatial distribution the south of Taiwan is greater than the northern. Kao [14] also combined the ground solar radiation measurements and photovoltaic (PV) systems observations to create a predicted model for the generated electric energy of photovoltaic systems. Though there are some researches on the properties of solar radiation and predicted solar energy, it is still not enough for the requirements of modern industrial needs. Now, we need accurate solar radiation forecasting in hours, days ahead. Therefore, we need numerical weather forecasting model to predict the coming solar radiation and photovoltaic energy. Due to the limitations of current NWP model, the cloud motion forecasting is still not accurate enough to conduct the solar energy forecasting. In the current development of solar energy forecasting in Taiwan, we focus on the Global Horizontal Irradiance (GHI) satellite retrievals and will make a qualified satellite-derived products to evaluate the GHI products from NWP model.

The objective of this research is to estimate the global horizontal irradiance distribution on the Taiwan areas and validate the satellite-derived GHI by the ground observations. Data set and processing was described in section 2. Methodology was explained in section 3. Section 4 will show the results and do some discussions. Finally, the conclusion and future works will be done in section 5.

2. Data set and processing

(a) MTSAT satellite

The satellite data used in this study is from Multifunctional Transport Satellite (MTSAT) gridded data provided by the Center for Environmental Remote Sensing, Chiba University, its ftp site is at ftp://mtsat.cr.chiba-u.ac.jp/grid-MTSAT-2.0. The specification of MTSAT is as follows : one visible channel centered at 0.725 μ m at four infrared (IR) channels centered at 10.8, 12.0, 6.75, and 3.75 μ m, respectively. The spatial resolutions of visible and IR channels are one and four km, respectively. The original MTSAT visible data set is a size of 12000 lines by 12000 samples with 0.01 by 0.01 degree grid size, ranging from 80.005 °E, 59.995 °N (upper left corner) to 159.995 °W, 60.005 °S) (lower right corner). Due to our interesting in Taiwan areas, only the data set between (119.0 $^{\circ}E$, 25.0 $^{\circ}N$) and (123.0 $^{\circ}E$, 21.25 $^{\circ}N$) are saved. The satellite visible data used in this study is from September of 2014 to August of 2015.

(b) The digital terrain model data

For pressure-corrected air mass, the digital terrain model data of Taiwan area are used in this study and its gridded size is interpolated to 0.01 by 0.01 degree for matching the same grid size with satellite visible data. The contour lines of terrain of Taiwan is shown in Figure 1. In the current status, we just use the following formula to finish the correction [15]

$$P_{s} = P_{o} e^{-0.000832H}$$
(1)

$$M_{p} = M \frac{P_{s}}{P_{o}}$$
(2)

where H, P_o , P_s , M, and M_p are terrain altitude, standard sea level pressure 1013.25 mob, station pressure, air mass and pressure-corrected air mass, respectively.



Figure 1 The image of digital terrain of Taiwan (Unit in meter).

(c) The Global Horizontal Irradiance data

The Global Horizontal Irradiance (GHI) ground observation data are provided by Central Weather Bureau in Taiwan and used to validate the satellite GHI retrievals. There are 31 ground solar radiation observation station in the Taiwan island and its neighbors. The distribution of station is shown in Figure 2.



Figure 2 The site distribution of ground solar radiation observation.The red circle symbols show the site locations. Stations with symbols A,B, C, and D are Taipei, Taichung, Tainan , and Hualien, respectively.

3. The Methodology

The semi-empirical satellite method was accepted in this study, its basic principle is that the fundamental observation that the visible Earth radiance seen by the satellite is approximately proportional to cloud opacity and to the cosine of solar-zenith angle [16]. There are two major parts needed to deal with : one is to find the clear sky irradiance background, and the other is to find the cloud attenuation superimposed on the background.

In the current status, for fast application usage, the Ineichen simplified SOLIS model was used in this study. This model is based on the typical exponential of direct beam irradiance:

$$DNI = I_o e^{(-t_b/\sin^0(e))}$$
(3)

where b is a parameter modified by air mass and the e is the elevation angle of sun. For the GHI, modification of the direct beam by the sine of the solar elevation provide a first estimation of the GHI as follows

$$GHI = I_o e^{\left(-t_g/\sin^g(e)\right)} \sin(e) \qquad (4)$$

where the parameter t_g is GHI optical depth. The results of regress analysis of I_0 , t_b , b, t_g , and g for elevations between sea level and 7 km, total precipitable water vapor from 0.2 to 10 cm, and aerosol optical depth between 0.0 and 0.45 were 1618, 0.606, 0.491, 0.464, and 0.402, respectively^[15].

(a) Cloud attenuation : cloud index

Before calculating the cloud attenuation, we should deal with the

digital count for every pixel to have the same solar view. The first step is to find its solar zenith angle and then correct the digital count by dividing cosine of solar zenith angle. The solar zenith angle is dealt with the following formula

$$\cos\theta_{o} = \sin\delta_{o}\sin\emptyset + \cos\delta_{o}\cos\emptyset\cosh$$
(5)

where θ_0 , δ_0 , \emptyset , h are solar zenith angle, solar declination angle, latitude of pixel, and hour angle, respectively. The solar declination angle used here is by Cooper [17]

$$\delta_{\rm o} = 23.45 \left[\frac{360(284 + N)}{365} \right] \tag{6}$$

where N is the day of year. The hour angle are 15 degrees per hour with negative value before solar noon and positive after solar noon.

The cloud index was defined as follows ^[15]

$$CI = \frac{CCC - CCLR}{CCLD - CCLR}$$
(7)

where CCLD, CCLR, and CCC are the digital count representing the deepest thickness of cloud, the digital count of clearest sky, and the cosine-corrected count, respectively, for a specific month in Taiwan area. The dynamic range of CCC is between 0 and 1024.

4. Results and Discussion

(a) The determination of CCLD and CCLR

Before determining the cloud index for each pixel of satellite

observation, we need to find one set of CCLD and CCLR values. For simplicity, here we just take one set values in the whole research area and all of the observation time. In the next step, we will find CCLD and CCLR values for a specific small area and short time period, month or season. Figure 3 is an example to find CCLD and CCLR values. It was found that the CCLRs vary with day, but the change is quite small. On the other hand, the variation of CCLRs are large, depending on the sky situations and cloud types and thickness.

Table 1 shows four different ground observation stations, Taipei (466920), Taichung (467490), Tainan (467410), and Hualien (466990), representing the northern, central, southern, and eastern parts of Taiwan, respectively, used for validation of satellite-derived GHIs.

(b) Pattern comparison of GHI

For understanding the accuracies of GHI satellite retrievals in a whole view, we compared the image of visible channel with that of satellite-derived GHI distribution to make sure the entire pattern is correct. Figure 4 shows the MTSAT visible image at 12:01L (local time) on June 1, 2015. It is a cloudy day case. There exist some thin clouds in the north, heavy clouds in the central mountain areas and

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relatively clear in the south. Figure 5 shows the distribution of satellite-derived GHI (W/m²) at the same time with Figure 4. The GHI is ranging between 200 and 600 W/m² in the north, 100-600 W/m² in the central mountain areas, 600-1100 W/m² in the south and east of Taiwan. It is very obvious that the two images have the same distribution pattern, and the GHI satellite retrievals are qualitatively reasonable. For quantitative evaluation, the ground solar observation data are used to compare with. At this time the ground GHI observations of Taipei, Taichung, Tainan, and Hualien stations are 344.4, 402.7, 836.1 and 538.9 W/m², respectively. The four points are located in the reasonable color bars.

(c) Quantitative comparison of GHI

In order to have an objective comparison between the satellite-derived and observed GHI. We use the whole month data of August, 2015. Table 2 shows the hourly ground GHI observation in August of 2015 at Taipei station. August is in the summer season with more sunny days. The ground GHI measurements are almost from 7 a.m. to 8 p.m.

Figure 6 shows the scatter diagram of satellite GHI retrievals and the solar ground observations at Taipei station for the whole month.

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The correlation coefficient between them is 0.8664 with 620 samples. This shows that there is a good relationship between them.

Figures 7, 8 and 9 are the same as Figure 6, but for Taichung, Tainan, and Hualien stations, and their correlation coefficients are 0.8540, 0.8990, and 0.8870, respectively. From the comparison of the four ground observations, it is evident that the quantitative evaluation of satellite-derived GHI is done well.



Figure 3 The sample of CCLD and CCLR determination by its digital count distribution in the research area. The lowest and the highest counts represent the clearest and the heavy cloudiness skies.

Table 1 Four ground observation stations' name, location and

Station	Station	Station altitude	Longitude	Latitude
name	code	(m)	(°E)	(°N)
Taipei	466920	7.0	121.5149	25.0377
Taichung	467490	85.0	120.6841	24.1457
Tainan	467410	41.0	120.2048	22.9932
Hualien	466990	16.0	121.6133	23.9751

altitude.

Figure 4 The MTSAT visible image at 12:01L on 2015/6/1.



Figure 5 The distribution of satellite retrieval GHI (W/m^2) at

12:01L on 2015/6/1.

Table 2 The hourly ground GHI observation of August, 2015 at Taipei

station.

				104	/8	С	WB	-46693	20(Ta:	ipei)	GHI g	ground	l obse	ervati	on			U	nit:W	/m^2						
day	hour 01	02	03	04	05	5	06	07	08	09	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	MAX
01		0 ()	0	0	0	0	136.14	375.08	569.57	786.29	825.18	997.45	1000.22	902.98	641.81	341.74	244.5	102.8	0	0	0	0	0	0	1000.22
02		0 ()	0	0	0	0	113.91	338.96	547.34	677.93	697.38	864.08	791.84	627.92	297.29	263.95	169.48	116.69	0	0	0	0	0	0	864.08
03		0 ()	0	0	0	0	119.47	272.28	561.24	766.84	891.87	741.83	769.62	650.15	202.82	375.08	166.7	77.8	0	0	0	0	0	0	891.87
04		0 ()	0	0	0	0	127.81	361.19	541.79	583.46	758.5	989.11	964.1	891.87	102.8	111.14	52.79	0	0	0	0	0	0	0	989.11
05		0 ()	0	0	0	0	125.03	352.86	555.68	647.37	616.8	972.44	733.5	402.87	38.9	80.57	125.03	108.36	0	0	0	0	0	0	972.44
06		0 (0	0	0	0	0	155.59	305.62	575.13	611.25	925.21	944.66	978	952.99	791.84	539.01	325.07	100.02	0	0	0	0	0	0	978
07		0 (0	0	0	0	0	86.13	316.74	641.81	736.28	941.88	655.7	830.74	494.56	527.9	261.17	94.47	5.56	0	0	0	0	0	0	941.88
08		0 ()	0	0	0	0	0	2.78	75.02	127.81	177.82	172.26	275.06	280.62	166.7	88.91	0	0	0	0	0	0	0	0	280.62
09		0 (0	0	0	0	0	0	0	83.35	250.06	502.89	430.65	494.56	219.49	172.26	169.48	166.7	5.56	0	0	0	0	0	0	502.89
10		0 ()	0	0	0	0	102.8	350.08	402.87	455.66	666.82	800.18	761.28	577.91	550.12	158.37	41.68	0	0	0	0	0	0	0	800.18
11		0 ()	0	0	0	0	144.48	341.74	552.9	744.61	694.6	897.42	925.21	661.26	405.65	8.34	0	0	0	0	0	0	0	0	925.21
12		0 ()	0	0	0	0	91.69	288.95	536.23	750.17	922.43	908.54	661.26	686.26	327.85	27.78	0	0	0	0	0	0	0	0	922.43
13		0 ()	0	0	0	0	69.46	366.75	555.68	733.5	908.54	989.11	508.45	33.34	0	8.34	122.25	33.34	0	0	0	0	0	0	989.11
14		0 ()	0	0	0	0	25.01	250.06	511.23	897.42	691.82	647.37	136.14	288.95	227.83	291.73	158.37	0	0	0	0	0	0	0	897.42
15		0 ()	0	0	0	0	22.23	252.83	530.67	666.82	777.95	822.41	672.37	294.51	333.41	238.94	166.7	47.23	0	0	0	0	0	0	822.41
16		0 ()	0	0	0	0	0	166.7	341.74	533.45	327.85	255.61	102.8	133.36	166.7	166.7	166.7	50.01	0	0	0	0	0	0	533.45
17		0 ()	0	0	0	0	0	52.79	227.83	297.29	441.77	275.06	708.49	564.02	436.21	294.51	177.82	66.68	0	0	0	0	0	0	708.49
18		0 ()	0	0	0	0	141.7	61.12	352.86	591.8	491.78	333.41	397.31	269.5	41.68	0	0	0	0	0	0	0	0	0	591.8
19		0 ()	0	0	0	0	133.36	369.53	589.02	780.73	922.43	964.1	847.41	905.76	680.71	280.62	305.62	108.36	0	0	0	0	0	0	964.1
20		0 ()	0	0	0	0	147.26	383.42	472.33	733.5	927.99	994.67	997.45	950.21	786.29	525.12	291.73	77.8	0	0	0	0	0	0	997.45
21		0 ()	0	0	0	0	130.58	344.52	583.46	605.69	847.41	1011.34	644.59	689.04	672.37	427.87	255.61	72.24	0	0	0	0	0	0	1011.34
22		0 (0	0	0	0	0	97.24	352.86	489	614.03	880.75	877.97	702.94	891.87	505.67	516.78	241.72	2.78	0	0	0	0	0	0	891.87
23		0 (0	0	0	0	0	0	113.91	91.69	347.3	280.62	180.6	380.64	480.66	144.48	72.24	13.89	0	0	0	0	0	0	0	480.66
24		0 ()	0	0	0	0	0	50.01	172.26	305.62	294.51	652.92	730.72	380.64	558.46	600.13	252.83	105.58	0	0	0	0	0	0	730.72
25		0 ()	0	0	0	0	0	0	0	188.93	277.84	500.11	394.53	427.87	602.91	372.31	200.04	11.11	0	0	0	0	0	0	602.91
26		0 ()	0	0	0	0	0	141.7	186.15	422.32	441.77	486.22	211.16	316.74	302.85	166.7	108.36	0	0	0	0	0	0	0	486.22
27		0 ()	0	0	0	0	0	0	125.03	211.16	338.96	505.67	141.7	0	0	0	61.12	0	0	0	0	0	0	0	505.67
28		0 ()	0	0	0	0	69.46	166.7	180.6	250.06	166.7	213.94	116.69	72.24	0	0	0	0	0	0	0	0	0	0	250.06
29		0 ()	0	0	0	0	0	0	155.59	166.7	372.31	591.8	558.46	230.61	122.25	77.8	0	0	0	0	0	0	0	0	591.8
30		0 ()	0	0	0	0	0	180.6	166.7	311.18	313.96	286.18	113.91	191.71	77.8	144.48	0	0	0	0	0	0	0	0	313.96
31		0 ()	0	0	0	0	0	83.35	113.91	83.35	86.13	94.47	150.03	91.69	58.35	77.8	63.9	0	0	0	0	0	0	0	150.03
AVE		0 0) (D	0	0	0	56.371	127.77	188.11	209.12	245.19	263.56	258.88	250.42	214.86	148.95	88.202	39.412	0	0	0	0	0	0	



Figure 6 The scatter diagram of GHI satellite retrievals verse the solar ground observations at Taipei station for August of 2015. The correlation coefficient between satellite retrievals and observation is
0.8664 with 620 samples.



Figure 7 Same as figure 6, but for the Taichung station. The

correlation coefficient between satellite retrievals and observation is

0.8540.





coefficient between satellite retrieval and ground observation is 0.8990.



Figure 9 Same as figure 6, but for the Hualien station. The correlation coefficient between satellite retrieval and ground observation is 0.8870.

Figure 10 shows the distribution of monthly satellite-derived GHI (MJ/m^2 * month) for August, 2015. The four points retrievals close to the Taipei, Taichung, Tainan, and Hualien observations, respectively, are 421.90, 384.70, 417.90, and 452.7 MJ/m^2. Table 6 lists the monthly ground GHI observation (MJ/m^2)from 2014/9 to 2015/8 for the four stations. Comparing the observations, the retrieval

values near the four stations are underestimated by 8.7 %, overestimated 0.6%, underestimated 8.8 %, and overestimated 1.7 %, respectively. The results show that the satellite-derived and ground observation values are quite consistent and the application of satellite retrievals in power management is feasible.



Figure 10 The distribution of monthly satellite-derived GHI (MJ/m² * month) for August, 2015.

Table 3The monthly ground GHI observation (MJ/m^2)from 2014/9to 2015/8 at Taipei, Taichung, Tainan, and Hualien stations.

Month	2014	2014	2014	2014	2015	2015	2015	2015	2015	2015	2015	2015
Station	/9	/ 10	/ 11	/ 12	/ 1	/ 2	/ 3	/ 4	/ 5	/ 6	/ 7	/ 8
Taipei	547.4	382.7	263.1	185.1	261.7	270.7	281.7	422.3	376.5	537.3	606.5	462.4
Taichung	458.3	488.2	337.4	260.8	364.3	363.1	369.8	516.2	392.6	549.5	489.4	382.3
Tainan	563.1	598.4	428.1	310.9	400.4	416.7	483.9	600.2	541.5	722.2	572.0	458.2
Hualien	532.5	377.0	276.2	138.1	198.3	220.2	275.6	342.7	446.7	601.4	606.8	445.0

5. Conclusions and future works

This study has successfully finished the GHI retrievals by MTSAT satellite data from a whole year dataset, September of 2014 to August of 2015. The distribution of satellite-derived GHI has the same pattern with that of ground observation. The point to point comparison also shows a good relationship between them. The correlation coefficients are all great than 0.85 for all four stations. Also, the monthly satellite GHI retrievals are all comparable with those of observations under 9% difference for the above four stations.

For the future power supply requirement, we need to forecast the

solar energy using numerical weather prediction model, like Weather Research and Forecasting (WRF) model. But in the current status the GHI forecasting is not good enough and need more improvement. Figure 11 is an example of GHI 36-hour forecasting at noon on June 1, 2016. It was shown that the forecast GHI values have a overestimation situation. The qualified satellite-derived GHI values are suitable for WRF model to improve its accuracy.

In the future, the Ineichen SOLIS model will replace the current simplified model, and the MODIS AOD products and total precipitable water vapor products will be put in the SOLIS model. This effort will improve the accuracy of GHI retrievals.



Figure 11 The distribution of GHI (W/m²) 36-hour forecasting by WRF model at 12:01L on 2015/6/1

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附件二:太陽天頂角訂正的Fortran程式碼: sla-correction.f

read MTSAT gridded file with 12000 lines by 12000 С samples and get

a subarea with 350 lines and 200 pixels per line. The С upper left

point is located at 22 degree N, 120 degree E. Grid size С is 0.01

* 0.01 degree. С

> character*37 fn character*16 fncor,monthcase character*17 fno

character*17 fnc

oimg is the original image С

cimg is the image after solar zenith angle correction С

coast is the position of coast line in image coordinate С system

С

С

parameter (ixmax=400, iymax=376) integer*1 oimg(ixmax,iymax) integer*1 cimg(ixmax,iymax) parameter (ipoint=888) integer ixcoast(ipoint), iycoast(ipoint) parameter (icasemax=1000) real corm(ixmax) integer*2 ny,nm,nd,inumday real sdecli, hangle, slat parameter (ireclraw=24000) the record length size is 24000 bytes, so there are 12000

```
2-byte-integer
С
      integer*2 m(12000)
      process many cases in one run
С
      write(*, *)'key in the month case name i.e.
С
(2014031ittle.1st)'
      read(5,80)monthcase
С
c80
       format(a16)
      open(15,file='little.lst',status='old')
      open(11, file='twcoast.dat', status='old')
c----read in the position of coast line in the image of
interesting
      do k5=1, ipoint
read(11,51)num, sslon, sslat, ixcoast(k5), iycoast(k5)
write(6,51)num, sslon, sslat, ixcoast(k5), iycoast(k5)
      enddo
51
      format(i5,2f10.3,2i5)
      run all the case in one month
C - - -
      do icase=1.icasemax
         read(15,25,end=99)fn
      open(unit=2, file=fn, status='old', form='unformatted',
           access='direct', recl=ireclraw)
     $
     taiwan range 25.005~21.775 N and 119.005~123.005 E
С
     line from 3450 to 3825 and pixel from 3401 to 3800
С
     taiwan image size is 376 lines * 400 pixel
С
      write(6, 10)fn
С
      read(fn(13:16), '(i4)'), ny
      read(fn(17:18), '(i2)'), nm
      read(fn(19:20), '(i2)'), nd
```

```
read(fn(21:22), '(i2)'), nh
      convert GMT to local time
С
      Taiwan areas located in the 120E, and need add 8 hours
С
      nh=nh+8
      read(fn(23:24), '(i2)'), nmin
      write(6,20)ny,nm,nd,nh,nmin
С
      fncor=fn(13:24)//'.cor'
      fno=fn(13:24)//'o.raw'
      fnc=fn(13:24)//'c.raw'
      open(10, file=fncor, status='unknown')
10
      format(5x, a42)
open(unit=25, file=fno, status='unknown', form='unformatted',
           access='direct', recl=400)
     $
open(unit=26, file=fnc, status='unknown', form='unformatted',
           access='direct', recl=400)
     $
20
      format(5x,5i6)
25
      format(a37)
      call dnum(ny,nm,nd,inumday)
      calculte the day number of year
С
      call declination(inumday, sdecli)
      call hourangle(nh,nmin,hangle)
      line=0
      slathigh=25.505
      do j=3450,3825
      line=line+1
      slat=slathigh-0.01*(line-1)
      call zenith(sdecli,slat,hangle,value,angle)
         read(2, rec=j) (m(jj), jj=1, 12000)
```

```
c----save origin image before solar zenith angle correction
         j1=0
         do kk=3401,3800,1
            j1=j1+1
            corm(j1)=m(kk)/value
c-- oimg is the origin image
c-- cimg is the image after solar zenith angle correction
            oimg(j1, line) = m(kk)/4
            cimg(j1,line)=int(corm(j1)/4)
            write(6,*)' slat j ori cor', slat,j1,
С
m(kk),corm(j1)
         enddo
         write(10,8)(corm(11),11=1,ixmax)
      enddo
c----replace the value of image in coastal line with the
account of -1
      do m10=1, ipoint
         ixx=ixcoast(m10)
         iyy=iycoast(m10)
         write(*,*)m10,ixx,iyy
         oimg(ixx, iyy) = -1
         cimg(ixx,iyy)=-1
      enddo
c----replace the value of longitutde of 120 E, 121 E, and 122
E with the account of -1
c---- the responcing ix are 100, 200, and 300
      do m11=1, iymax
         oimg(100, m11) = -1
         cimg(100, m11) = -1
         oimg(200, m11) = -1
```

```
cimg(200, m11) = -1
          oimg(300, m11) = -1
          cimg(300, m11) = -1
       enddo
c----replace the value of latitude of 24 \text{ N}, 23 \text{ N} and 22 \text{ N} with
the account of -128
c---- the responding iy are 151, 251 and 351
       do m12=1, ixmax
          oimg(m12, 51) = -1
          cimg(m12, 51) = -1
          oimg(m12, 151) = -1
          cimg(m12, 151) = -1
          oimg(m12, 251) = -1
          cimg(m12, 251) = -1
          oimg(m12, 351) = -1
          cimg(m12, 351) = -1
       enddo
c---- output the original and solar zenith angle correction
images with
      coast line
С
       do m20=1, iymax
      write(25, rec=m20)(oimg(m7, m20), m7=1, ixmax)
      write(26, rec=m20)(cimg(m8, m20), m8=1, ixmax)
       enddo
       close(2)
       close(10)
       close(25)
       close(26)
       enddo
      format(400f7.1)
8
```

84

99 stop end subroutine dnum(iy,m,id,numday) calculate the day number of year С For Feb. there are 29 days for leap year and the other С is only 28 days С if the year can be the divided by 4 and 400 completely, С then the year is laep year С integer*2 numacc(12),n1,n2,iy,m,id data numacc/31,59,90,120,151,181,212,243,273,304,334,365/ n1=mod(iy,4)n2 = mod(iy, 400)if(n1 .eq. 0 .and. n2 .eq. 0)then numday=numacc(m-1)+id+1 else numday=numacc(m-1)+id endif return end subroutine declination(knumday,sdec) the solar declination angle is calculated by the С

```
following formula
```

the author is Cooper, 1969
real sdec,d2rc
pi=4.0*atan(1.0)
d2r=pi/180.0
sdec=23.45*sin((360.0/365.0)*(knumday+284)*d2r)
return
end

subroutine hourangle(kh,kmin,hang)

```
c calculate hour angle
```

c in the morning the hour angle is positive

- c and in the afternoon negative
- c one hour correspond to 15 degrees

С

С

```
if (kh. lt. 12)then
hang=15.0*(12-kh-(kmin/60.0))
else
hang=-15.0*(kh-12+(kmin/60.0))
endif
return
end
```

c calculate the zenith angle for the viewing point subroutine zenith(solarde,rlat,ha,cosvalue,ze) pi=4.0*atan(1.0) d2r=pi/180.0 r2d=180.0/pi cosvalue=sin(solarde*d2r)*sin(rlat*d2r)+ * cos(solarde*d2r)*cos(rlat*d2r)*cos(ha*d2r)

```
ze=acos(cosvalue)*r2d
c write(6,*)'value zenith_angle',cosvalue,ze
return
end
```